

Electrical Submersible Pump Design in Vertical Oil Wells

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Abstract

Artificial Lift is a very essential tool to increase the oil production rate or lift the oil column in the wellbore up to the surface. Artificial lift is the key in case of bottom hole pressure is not sufficient to produce oil from the reservoir to the surface. So, a complete study is carried to select the suitable type of artificial lift according to the reservoir and wellbore conditions like water production, sand production, solution gas-oil ratio, and surface area available at the surface. Besides, the maintenance cost and volume of produced oil have an essential part in the selection of the type of artificial lift tool. Artificial lift tools have several types such as Sucker Rod Pump, Gas Lift, Hydraulic Pump, Progressive Cavity Pump, Jet Pump, and Electrical Submersible Pump. All these types require specific conditions for subsurface and surface parameters to apply in oil wells. This paper will study the Electrical Submersible Pump "ESP" which is considered one of the most familiar types of artificial lifts in the whole world. Electrical Submersible Pump "ESP" is the most widely used for huge oil volumes. In contrast, ESP has high maintenance and workover cost. Finally, this paper will discuss a case study for the Electrical Submersible pump "ESP" design in an oil well. This case study includes the entire well and reservoir properties involving fluid properties to be applied using Prosper software. The results of the design model will impact oil productivity and future performance of oil well.

Keywords: Submersible; Pump; Design; PROSPER; Artificial Lift; Oil Well

Introduction

Artificial lift is considered the backbone for enhancement productivity from oil wells in the world. Selecting the optimum artificial lift technique represents a challenge for the petroleum production engineer. Petroleum engineer could arrange the optimum type of artificial lifts according to technical and economical evaluation [1,2]. In addition, the reservoir drive mechanism has an important role in the selection of optimum type of artificial lifts. Therefore, in case of depletion drive mechanism with high initial oil rate in the early production life of reservoir, the optimum type of artificial lift is continuous gas lift or electrical submersible pump "ESP" could be applied. In contrast, with production time there are steep decrease in reservoir pressure, therefore the rate of produced fluid is decreased that requires to change the type of artificial lift tool to be intermittent gas lift or Sucker rod pump that run on oil wells having low productivity [3].

In case of bottom hole pressure is unable to lift fluids to the surface due to the reservoir pressure has been declined rapidly with excessive water production. Therefore, it is considered the optimum time to run artificial lift tools. These artificial lift tools could overcome the loss in reservoir pressure, which will help to increase drawdown due to reducing the bottomhole flowing pressure against sand face of the formation. The reduction in bottomhole flowing pressured leads to increase difference in pressure between reservoir and wellbore and increase in oil production rate as shown in Figure 1 [4,5].



There are different types of artificial lift tools with different specifications related to well parameters, reservoir and fluid properties. Each type of artificial lifts has different advantages and limitations according to its application on oil well. The artificial lifting tools include gas lift, Sucker Rod Pump, Hydraulic Pump, Progressive Cavity Pump and Electrical Submersible Pump [6-8]. There are many parameters affecting the selection of the optimum type of artificial lifting techniques that include reservoir, wellbore, surface and operation parameters.

The reservoir parameters are production rate, water production rate, solution gas oil ratio, oil viscosity, oil formation volume factor, inflow performance relationship, and the driving mechanism.

The surface conditions include location of field, power source, surface production rate, and contamination of fluids. The conditions of field operation are plan for pressure maintenance, plan for long life recovery, surface facility, and plan for enhanced oil recovery. The wellbore parameters include total depth of the well, type of completion in the well, tubing and casing diameter, and deviation of wellbore [9,10].

Operating Conditions for Artificial Lift tools

Different Types of artificial lift tools have been applied on oil wells according to reservoir, wellbore and surface conditions that each type of artificial lifts has some conditions are favorable to apply in addition to the components of reservoir production as presented in Table 1[11].

Operating Conditions	Rod Pump	Hydraulic Pump	Electric Submersible Pump	Gas Lift
Sand	Fair	Fair	Fair	Excellent
Paraffin	Poor	Good	Good	Poor
High Gas oil ratio	Fair	Fair	Fair	Excellent
Deviated Hole	Poor	Good	Fair	Good
Corrosion	Good	Good	Fair	Fair
High Volume	Poor	Good	Excellent	Good
Depth	Fair	Excellent	Fair	Good
Flexibility	Fair	Excellent	Poor	Good
Scale	Good	Fair	Poor	Fair

Table 1: Comparison between all types of artificial lifts.

Electrical Submersible Pump

Electrical Submersible Pump is the most familiar and widely used in the petroleum industry in the world which more than 100000 oil wells are using electrical submersible pump in the world in order to lift the fluids to the surface or in order to accelerate the well production. This type of Pump is familiar in handling huge quantity of fluids to the surface even if high amount of water produced with oil. The major components of this type of pump is multistage centrifugal pump is attached to downhole motor by shaft. Heavy cable is delivered from the surface to downhole motor in order to deliver the electricity. In addition, there are downhole motor in order for further protection as shown in Figure 2 [12,13].



Pump.

Advantages of Electrical Submersible Pump [9,14]

- 1. Electrical Submersible Pump can provide large produced liquid volume from the reservoir
- 2. Electrical Submersible Pump has only limited equipment at the surface
- 3. Electrical Submersible Pump is highly recommended in highly deviated wells and in wells with severe dogleg.
- 4. Electrical Submersible Pump efficiency is very high that produce greater than 1000 bbl/day liquid.
- 5. Electrical Submersible Pump has high resistance to corrosion in oil wells.
- 6. Electrical Submersible Pump has low cost of maintenance.

Limitations of Electrical Submersible Pump [9,15]

- 1. Electrical Submersible Pump has a great problem in case of sand production from reservoir to the wellbore.
- 2. Electrical Submersible Pump has a great problem in case of high gas oil ratio is produced from the reservoir or in case of high bottom hole pressure in some oil wells with great depth.
- 3. Electrical Submersible Pump is difficult to use in case of low oil production from some wells. In case of production is lower than 200 barrel per day.
- 4. Electrical Submersible Pump is very critical in case of oil wells in the offshore area.
- 5. Electrical Submersible Pump requires large diameter of casing in case of high volume of liquid produced from the reservoir.
- 6. Electrical Submersible Pump is very costly in case of there is a failure in the downhole motor.

There are several softwares designed to build a model for electrical submersible pump for any oil well according to several conditions. These conditions such as reservoir properties, well parameters and surface conditions could enable us to select the best and optimum Electrical Submersible Pump parameters that match all conditions in order to enhance well performance and increase well productivity. One of the main parameters is gas oil ratio that influence on number of stages in ESP pump. Increasing gas oil ratio that produced from the reservoir will increase number of stages in the pump. One of the most familiar and widely used software is PROSPER that could select the optimum design for electrical submersible pump for all oil wells conditions [16].

There are some constrains for electrical submersible pump such as sand production from reservoir to the wellbore. In these conditions, downhole screen or filter has to be installed against the formation intervals in order to prevent any wear in the downhole pump. So, most of wells that have sand production, also have gravel pack in order to protect downhole motor from sand. However, most of artificial lift tools could not handle sand production from reservoir to the wellbore. There are only two types of artificial lift tools could handle sand production. These two types are gas lift and progressive cavity pump [12].

Design of Electrical Submersible Pump

Table 2 presents the reservoir and fluid properties for an oil well is producing from black oil reservoir has low productivity due to losses in wellbore pressure from sand face to the surface. Therefore, it is planned to design Electrical submersible pump to maximize oil productivity from well. The reservoir has high oil potential and large oil volume could deliver to the well bore which requires an artificial lift tool to produce large volume of oil production to the surface. The benefit of Electrical submersible pump is producing large liquid volume because it has the ability to carry large quantity of liquid to the surface. Figure 3 displays the input fluid properties in order to match the reservoir data.

Use Tables		Export	
Input Parameters			Correlations
Solution GOR	800	scf/STB	Pb, Rs, Bo Glaso
Oil Gravity	35	API	Oil Viscosity Beal et al
Gas Gravity	0.78	sp. gravity	
Water Salinity	80000	ppm	
Impurities			Pump Data
Mole Percent H2S	0	percent	
Mole Percent CO2	0	percent	
Mole Percent N2	0	percent	

Figure 3: Input	: PVT Data i	in PROSPER	software.
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Reservoir pressure, psi	5200
Bubble point pressure, psi	3600
Reservoir Temperature, F	250
GOR, scf/stb	800
Water cut, %	50
API	35
Gas specific gravity	0.78
Water salinity, ppm	80,000
Oil FVF, bbl/stb	1.45
Oil viscosity, cp	0.3

Table 2: Reservoir and fluid properties.

This PVT data have to be matched with the matching parameters using the suitable correlation in PROSPER model. There are several correlations could be applicable. Prosper software will make a lot of iterations in order to achieve the best correlation that will represent the reservoir fluid properties. Figure 4 depicts the matching parameters have to be matched with fluid properties.

Dor	ne Main	Cancel	Reset Cop	y Clip	Import	PVTP Import	Transfer	Plot	Help
٩VT	Match data								
	Table		Temperat Bubble Pi	ure 250 bint 3600	deg psig	F			
	Pressure	Gas Oil Ratio	Oil FVF	Oil Viscosity					
	psig	sef/STB	RB/STB	centipoise					
1	3600	800	1.456	0.31					
2									
3									
4									
5									
6									
7			<u> </u>	<u> </u>					
8			<u> </u>						
9		<u> </u>		<u> </u>					
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Figure 4: Matching parameters for fluid properties.

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Bubble Point						
	Glaso	Standing	Lasater	Vazquez-Beggs	Petrosky et al	Al-Marhoun
Parameter 1	91.278	1	41.3206	91.1376	1	90.9341
Parameter 2	3613.91	0	1192.78	3417.82	0	3068.47
Std Deviation	0.49		0.12	0.35	ļ	0.31
	Reset	Reset	Reset	Reset	Reset	Reset
Solution GOB						
0000110011	Glaso	Standing	Lasater	Vazquez-Beggs	Petrosky et al	Al-Marhoun
Parameter 1	-1163.69	-1193.58	0.80667	-1419.42	1	1
Parameter 2	1713.51	1716.47	-0.19129	1738.8	0	0
Std Deviation	565.615	565.615	ĺ	565.615	1	
	Reset	Reset	Reset	Reset	Reset	Reset
/// //	Glaso	Standing	Lasater	Vazquez-Beggs	Petrosky et al	Al-Marhoun
Parameter 1	0.99755	1	0.8968	1	0.99372	1
Parameter 2	-0.0024577	0	0.1015	0	-0.0063582	0
Parameter 3	1	1	1	1	1	1
Parameter 4	1e-8	0	1e-8	0	1e-8	0
Std Deviation	0.28274		1	Ĭ	0.31763	
	Reset	Reset	Reset	Reset	Reset	Reset
Ul Visconitur		Beggs et al	Petrosky et al	Egbogah et al	Bergman-Sutton	
)il Viscosity	Beal et al					
lil Viscosity Parameter 1	Beal et al 0.70398	0.53063	0.87085	1.43344	2.49092	
il Viscosity Parameter 1 Parameter 2	Beal et al 0.70398 -0.22479	0.53063	0.87085	1.43344 -9.16069	2.49092	
Dil Viscosity Parameter 1 Parameter 2 Std Deviation	Beal et al 0.70398 -0.22479	0.53063 -2.44054 1e-6	0.87085	1.43344 -9.16069 2e-6	2.49092 -13.7265	

Figure 5: Different correlations selection for matching parameters.

The best correlation will be selected depending on two parameters. The first parameter must be closest to one in value while, the second parameter must be near to zero in order to achieve the lowest standard deviation. Figure 5 shows the different correlations used in PROSPER model. The best correlation for calculating solution gas oil ratio, bubble point pressure and oil formation volume factor is Glaso correlation where, Beal et al. correlation is the best on for calculating the oil viscosity. These correlations will be applied to predict the future performance of reservoir fluid.

Inflow Performance Relationship

Inflow performance relationship "IPR" represents the performance of reservoir to deliver liquid to the wellbore. In order to establish the inflow performance relationship, it is required to import reservoir parameters depending on reservoir model selected such as reservoir pressure, reservoir temperature, water cut from reservoir, gas oil ratio and productivity index of reservoir. Then plot inflow performance of reservoir as shown in Figure 6.



Figure 6: Model selection and required parameters for IPR.



PROSPER software will use the above reservoir parameters to calculate the inflow performance relationship at different pressure values then plot this inflow performance on curve that will be illustrated in Figure 7.

Vertical Lift Performance Data

There are several parameters will control the value of pressure losses in the well such as deviation survey which represents the change in well trajectory regarding to the vertical depth of the well. Figure 8 displays the input data for deviation survey on PROSPER model.

Downhole equipment represents the different sizes of each equipment in the well bore that may cause pressure loss due to the obstruction of different sizes in the well bore. Figure 9 shows the input equipment in this case study.

Geothermal Gradient represents the change in temperature with depth, as it will have an impact on the well productivity and well bore pressure. Figure 10 illustrates the input temperature change with depth in the wellbore.

Done	: Cancel	Main	Help	Filter
Input Da	ita			
	Measured Depth	True Vertical Depth	Cumulative Displacement	Angle
	(feet)	(feet)	(feet)	(degrees)
1	0	0	0	0
2	1000	1000	0	0
3	1500	1500	0	0
4	1954	1950	60.1332	7.6113
5	2262	2250	129.876	13.0873
6	3077	3000	448.819	23.038
7	8993	8000	3610.95	32.3103
8	12672	11000	5740.51	35.3692
9	12960	11200	5947.74	46.017
10	13435	11500	6316.01	50.8333
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12				
13				
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MD cos	TVD			
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			Calculat	e



Figure 9: Well Downhole Equipment.

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npu	t Data					
	F	ormation	Forma	tion	Ove	erall Heat
	meas	(feet)	ídea	F)	Co	efficient
1	0		60	<u> </u>	BTU	J/h/ft2/F
2	1000		50]	8.24	
3	1340	0	250			
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After constructing the inflow performance relationship that represents the reservoir deliverability, the design of electrical submersible pump requires several input parameters in order to evaluate the efficiency of electrical submersible pump and calculate the different outputs.

There are several input parameters are required to design electrical submersible pump. These parameters such as depth of pump, length of power cable, required rate, reservoir water cut, gas oil ratio of reservoir, top node pressure. The input parameters have been imported in PROSPER software as shown in Figure 11.

alculate Design Done	Cancel	Report Export Hel
ut Data		_
Pump depth (Measured)	12000	feet
Operating Frequency	60	Hertz
Maximum OD	6	inches
Length Of Cable	13500	feet
Gas Separator Efficiency	0	percent
Design Rate	12000	STB/day
Water Cut	80	percent
Total GOR	800	scf/STB
Top Node Pressure	350	psig
Motor Power Safety Margin	0	percent
Pump Wear Factor	0	fraction
Pipe Correlation	Beggs and	d Brill
Tubing Correlation	Petroleum	Experts 3 1.00 1.00
Gas DeBating Model	(nono)	

Figure 11: Data required for electrical submersible pump design.

Results of Electrical Submersible Pump Design

By using the input parameters, PROSPER software could calculate the pump intake pressure, pump discharge pressure, pump discharge rate, actual head required as shown in Figure 12.

Done Calculate	Main	Help	Export	Sensitivity	
Flowing Bottomhole Pressure	3352.25	(psig)			,
Water Cut	80	(percent)			
Pump Frequency	60	(Hertz)			
Pump Intake Pressure	2941.35	(psig)			
Pump Intake Temperature	249.012	(deg F)			
Pump Intake Rate	13787.6	(RB/day)			
Free GOR Entering Pump	182.314	(scf/STB)			
Pump Discharge Pressure	4510.68	(psig)			
Pump Dischage Rate	13479.2	(RB/day)			
Total GOR Above Pump	800	(scf/STB)			
Mass Flow Rate	4378361	(lbm/day)			
I otal Fluid Gravity	0.91992				
Average Downhole Hate	13577.5	(RB/day)			
Head Hequired	3939.01	(reet)			
Actual Head Required	3939.01	(reet)			_
Fluid Power Required	361.707	(np) (fraction)			
Cas Fuerfump Intake (V/V)	0.034730	(naction)			
dias Fraction At Pump Intake	0.055627	(maction)			

Figure 12: Calculations required to design the electrical submersible pump.

Finally, PROSPER could design the optimum parameters and output of electrical submersible pump that will be applied in this well. The results of PROSPER for electrical submersible pump design are number of pump stages equal 106 stage, required power equal 571 hp, the outlet temperature of the pump equal 255 F and the efficiency of electrical submersible pump equal 64 %. Figure 13 illustrates the results of electrical submersible pump design by PROSPER software for this well. The operating area of electrical submersible pump is shown in Figure 14.

Done Cancel	Mair	n Help	Plot		
ut Data					
Head Required	3939.01	feet	Pump Intake Pressure	2941.35	psig
Average Downhole Rate	13577.5	RB/day	Pump Intake Rate	13787.6	RB/day
Total Fluid Gravity	0.91992	sp. gravity	Pump Discharge Pressure	4510.68	psig
Free GOR Below Pump	182.314	scf/STB	Pump Discharge Rate	13479.2	RB/day
Total GOR Above Pump	800	scf/STB	Pump Mass Flow Rate	4378361	lbm/day
Pump Inlet Temperature	249.012	dea F	Augrage Cable Temperature	220.493	dea F
Select Pump	CENTRILIF	T KC12000 5.62 incl	hes (9500-14500 RB/day)	220.403	ucyi
Select Pump Select Motor Select Cable		T KC12000 5.62 incl	Avelage Cable reinperdure	220.400	ucgi
Select Pump Select Motor Select Cable	CENTRILIF	T KC12000 5.62 incl	Average Cable Feinperaute	220.403	ucgi
Select Pump Select Motor Select Cable suits Number Of Stages		T KC12000 5.62 incl	Average Cable Tellipendue hes (9500-14500 RB/day) Motor Efficiency	220.403	percent
Select Pump Select Motor Select Cable suits Number Df Stages Power Required	CENTRILIF 106 571.412	r KC12000 5.62 incl	Metage Cable Telliperature hes (9500-14500 RB/day) Motor Efficiency Power Generated	220.400	percent hp
Select Pump Select Motor Select Cable sults Number Of Stages Power Required Pump Efficiency	CENTRILIF	KC12000 5.62 incl	Metage Cable Telliperature tes (9500-14500 RB/day) Motor Efficiency Power Generated Motor Speed		percent hp rpm
Select Pump Select Motor Select Cable suits Number DI Stages Power Required Pump Efficiency Pump Utilet Temperature	CENTRILIF	KC12000 5.62 incl	Average Cable Telligenature hes (9500-14500 RB/day) Motor Efficiency Power Generated Motor Speed Voltage Drop Along Cable		percent hp rpm Volts
Select Pump Select Motor Select Cable suits Number Of Stages Power Required Pump Dutlet Temperature Qurep 1 Ised	CENTRILIF	r KC12000 5.62 incl	Average Cable Telliperature hes (9500-14500 RB/day) Motor Efficiency Power Generated Motor Speed Voltage Drop Along Cable Voltage Drop Along Cable		perce hp rpm Volts Volts





Conclusions

An electrical submersible pump was designed for an oil well to enhance the well productivity and improve the well performance. The results of ESP design in Prosper software indicated the operating area of pump, the pump efficiency, and number of stages required to lift liquid volume to the surface. The results of PROSPER for electrical submersible pump design are number of pump stages equal 106 stage, required power equal 571 hp, the outlet temperature of the pump equal 255 F and the efficiency of electrical submersible pump equal 64 %.

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